

IN THE SPECIFICATION:

Please amend the paragraph starting at page 19, line 5 to page 20, line 5 as follows:

--The light deflector 4 can produce a high light converging effect and to consequently provide a light source device with an enhanced degree of luminance when a vertex split angle α of the first prism face 44 is 2 to 25 degrees and a vertex split angle β of the second prism face 45 is 33 to 40 degrees, an absolute value of the difference between α and β ($|\alpha - \beta|$) being 8 to 35 degrees. For the purpose of the present invention, the vertex split angles α , β denote respectively the left and right split angles of the vertex angle of each of the elongated prisms relative to the direction of the normal of the elongated prism forming plane 43, the angle between the first prism face 44 and the normal of the elongated prism forming plane 43 at the vertex (VER) of the elongated prism being referred to as α , the angle between the second prism face 45 and the normal of the elongated prism forming plane 43 at the vertex of the elongated prism being referred to as β . Additionally, it is possible to achieve a very high luminance by arranging two or more surfaces for the prism face in such a way that closer to the light output surface 42, greater the angle of inclination for the surfaces and making the peak angles of lights totally reflected by the respective surfaces and emitted from the light output surface 42 agree with each other for all the surfaces. At this time, the difference between the angle of inclination of the surface located closest to the light output surface and the angle of inclination of the surface located remotest from the light output surface is found within a range between 1 and 15 degrees, preferably between 5 and 12 degrees, more preferably between 7 and 10 degrees. It is possible to design a light deflector showing desired light converging characteristics with ease and manufacture a light deflector showing given optical characteristics on a stable basis by making the second prism face

45 show such a configuration.--

Please amend the paragraph starting at page 24, line 22 to page 25, line 20 as follows:

--As specific profiles of the elongated prism, if (x, z) coordinate system is adopted in which a vertex of each of the elongated prisms is assumed to be an origin of the coordinate system and a length of a pitch P of the elongated prisms is normalized to 1, the elongated prism may preferably have fifteen (15) planar surfaces and show a cross section formed by connecting in order the adjacent two of sixteen (16) points (p1-p16 in Fig. 21) of point 1 (-0.111, 1.27), point 2 (0.0, 0.0), point 3 (0.159, 0.195), point 4 (0.212, 0.260), point 5 (0.265, 0.328), point 6 (0.319, 0.398), point 7 (0.372, 0.470), point 8 (0.425, 0.544), point 9 (0.478, 0.621), point 10 (0.531, 0.699), point 11 (0.584, 0.780), point 12 (0.637, 0.861), point 13 (0.690, 0.945), point 14 (0.743, 1.030), point 15 (0.796, 1.117) and point 16 (0.889, 1.27). Alternatively, the elongated prism may have eleven (11) planar surfaces and show a cross section formed by connecting in order the adjacent two of twelve (12) points (p1-p12 in Fig. 23) of point 1 (-0.284, 1.059), point 2 (0.000, 0.000), point 3 (0.212, 0.278), point 4 (0.265, 0.350), point 5 (0.319, 0.423), point 6 (0.372, 0.501), point 7 (0.425, 0.581), point 8 (0.478, 0.663), point 9 (0.531, 0.748), point 10 (0.584, 0.834), point 11 (0.637, 0.922) and point 12 (0.716, 1.059). Still alternatively, the elongated prism may have twelve (12) planar surfaces and show a cross section formed by connecting in order the adjacent two of thirteen (13) points (p1-p13 in Fig. 22) of point 1 (-0.206, 1.168), point 2 (0.000, 0.000), point 3 (0.159, 0.204), point 4 (0.212, 0.273), point 5 (0.265, 0.343), point 6 (0.319, 0.416), point 7 (0.372, 0.490), point 8 (0.425, 0.567), point 9 (0.478, 0.646), point 10 (0.531, 0.727), point 11 (0.584, 0.810), point 12 (0.637, 0.897) and point 13

(0.794, 1.168).--

Please amend the paragraph starting at page 25, line 21 to page 26, line 5 as follows:

It is not necessary to form the above mentioned cross section so as to rigorously pass through all the sixteen (16) points, twelve (12) points or thirteen (13) points. Little displacement from each of the points (to pass through their neighborhood points) does not significantly affect the intensity of peak light. However, when the length of the pitch P of the elongated prisms is normalized to 1, it is desirable that the displacement of each of at least five (5) points in the sixteen (16) points, twelve (12) points or thirteen (13) points is such that the displaced point is found inside a circle (CIR in Figs. 21-23) centered at the corresponding proper point with a radius of 0.021, preferably with a radius of 0.018, more preferably with a radius of 0.014. It is most desirable that the displacement of each of eight (8) points is such that the displaced point is found inside a circle with a radius of 0.014.--

Please amend the paragraph starting at page 27, line 19 to page 28, line 10 as follows:

--As for the relationship between the pitch P of the elongated prisms and the length L2 of the virtual straight line (V) connecting the vertex (VER) and the trough section (TRO) of the elongated prism to each other in a cross section thereof as to the prism face 45, they preferably show a relationship of $L2 / P = 1.1$ to 1.7 for the purpose of increasing the quantity of light the prism face 45 receives, directing the angle of peak light in the distribution of the emitted light which has been internally reflected by each of the areas of the prism face of each elongated prism to the normal and preventing the vertex angle ($\alpha + \beta$) of the elongated prism from becoming too

small. The relationship is expressed by $L2 / P = 1.16$ to 1.6 more preferably, by $L2 / P = 1.27$ to 1.56 most preferably. As for the relationship between the length $L1$ of the virtual straight line connecting the vertex and the trough section of the elongated prism to each other in a cross section thereof as to the prism face 44 and the length $L2$ of the virtual straight line connecting the vertex and the trough section of the elongated prism to each other in a cross section thereof as to the prism face 45, the relationship is expressed preferably by $L2 / L1 = 1.1$ to 1.3 , more preferably by $L2 / L1 = 1.13$ to 1.25 , most preferably by $L2 / L1 = 1.16$ to 1.22 .

Please amend the paragraph starting at page 29, line 9 to page 30, line 20 as follows:

--When the length of the pitch P of the elongated prisms is normalized to 1, the edge line (EL in Fig. 24) formed by the two prism faces of each elongated prism may be undulated by 0.018 to 0.354 relative to the base line (BL in Fig. 24) (located at the average height of the elongated prisms) for the edge line, preferably by 0.018 to 0.177 , more preferably by 0.018 to 0.088 , most preferably by 0.035 to 0.063 . With such an arrangement, in a light deflector according to the invention that can converge incident light and emit it highly intensively in the viewing direction, it is possible to prevent glaring light viewed when a liquid crystal display element is observed after a light close to a collimated light is incident on the liquid crystal display element from appearing and make the defect of the light guide and that of the light deflector visually unclear to consequently minimize the uneven distribution of luminance to improve the quality of the light source device by forming undulations on the edge line in the Z-direction. On the other hand, a slight gap is produced between the light guide and the light deflector when undulations are formed on the edge line. Then, there is light emitted from the

light guide which strikes the elongated prisms located at the side opposite to the primary light source relative to the elongated prism that the emitted light strikes when such a gap is not produced. Then, light emitted from the light guide in a direction close to the normal relative to emitted peak light may not strike the main reflection surface (the prism face remote from the primary light source) to consequently reduce the overall luminance to a corresponding extent. However, a light deflector according to the present invention is adapted to raise the luminance to a large extent, compensating the reduction in the luminance due to the undulations of the edge line, and consequently prevent the overall luminance reduction of the light deflector from occurring. For a light deflector according to the invention to satisfactorily realize its advantages, it is preferable to confine the undulations of the edge line to the above cited range. The method for forming undulations on the edge line is not subjected to any particular limitations. For example, there may be used a method of forming the light deflector with use of a lens mold manufactured by cutting a lens pattern on a surface thereof while applying specific vibrations or a method of forming the light deflector by grinding the edge line section of each elongated lens of a known lens sheet by means of fine sand paper, etc.--

Please amend the paragraph starting at page 30, line 21 to page 31, line 22 as follows:

--When the length of the pitch P of the elongated prisms is normalized to 1, the quality of the light deflector can be improved by forming undulations on the two prism faces of each elongated prism by 0.012 to 0.334 relative to their respective base planes (BP1, BP2 in Fig. 25) (plane each including both the base line of the edge line and the bottom (BOT in Fig. 2) of the prism face (edge at the trough section side)) as in the case of forming undulations to the edge

line. The extent of undulations relative to the base planes is preferably 0.012 to 0.152, more preferably 0.012 to 0.076, most preferably 0.022 to 0.046.--

Please amend the paragraph starting at page 31, line 23 to page 32, line 14 as follows:

--When one of the prism faces is formed by a plurality of planar surfaces or convex curved surfaces with different angles of inclination in the light deflector 4 having the above described configuration, in order to secure sufficient light converging performance, the ratio (d/P) of the maximum distance (d) between the virtual plane (Q in Fig. 2) connecting the vertex (VER) and the bottom (BOT) of each elongated prism to each other and the plurality of planar surfaces or convex curved surfaces (actual prism face) relative to the pitch (P) of the elongated prisms is preferably 0.4 to 5%. This is because the light converging performance tends to be degraded to make it difficult to sufficiently improve the luminance when the ratio of d/P is lower than 0.4% or higher than 5%. More preferably, the ratio of d/P is within a range between 0.4 and 4.5%, most preferably between 0.7 and 4.0%. The ratio (r/P) of the radius of curvature (r) of the convex curved surface relative to the pitch (P) of the elongated prisms is preferably within a range between 2 and 50, more preferably within a range between 5 and 30, most preferably within a range between 6.5 and 12. This is because the light deflector cannot exhibit a sufficient light converging performance and the luminance tends to fall when the ratio of r/P is lower than 2 or higher than 50.--